

# Shear Band Direction in Amorphous Solids

- "An Atomistic Theory"

**Ashwin J.**

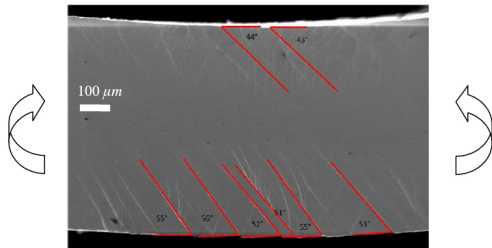
Institute for Plasma Research, Bhat Village, Gandhinagar-382428, India.

**H.G.E Hentchel, O. Gendelman, C. Shor & I. Procaccia**

January 2014

# The Puzzle

“At high enough strains, amorphous solids undergo plastic failure via spontaneous strain localization along a shear band, the direction of which **depends strongly** on loading protocols.”



Bending experiment<sup>1</sup> on a plate of  $\text{Zr}_{52.5}\text{Al}_{10}\text{Ti}_5\text{Cu}_{17.9}\text{Ni}_{14.6}$

<sup>1</sup>Y. F. Gao et al, *Acta Materialia* (59) 4159 (2011)

# Plan of the talk

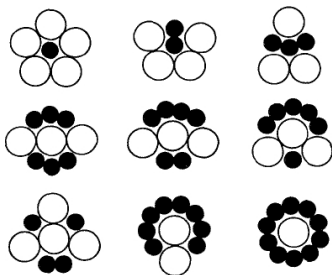
- ▶ Numerical simulations.
- ▶ Atomistic theory of plastic deformation.
- ▶ Comparison with simulations & experiments.
- ▶ Summary & road ahead.

# Model glass former used

- ▶ Binary Lennard-Jones system:

$$U(r) = 4\epsilon_{\alpha\beta} \left[ \left( \frac{\lambda_{\alpha\beta}}{r} \right)^{12} - \left( \frac{\lambda_{\alpha\beta}}{r} \right)^6 \right]$$

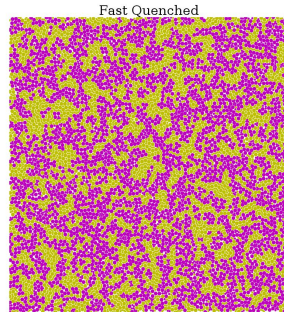
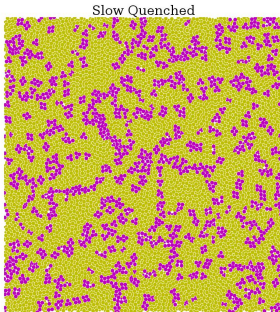
$\epsilon_{\alpha\beta}$  and  $\lambda_{\alpha\beta}$  are chosen for **quasi-crystalline**<sup>1</sup> ground state.



<sup>1</sup>M. Widom, K. J. Strandburg, and R. H. Swendsen, PRL (58), 706 (1987)

# Cooling a liquid into glass

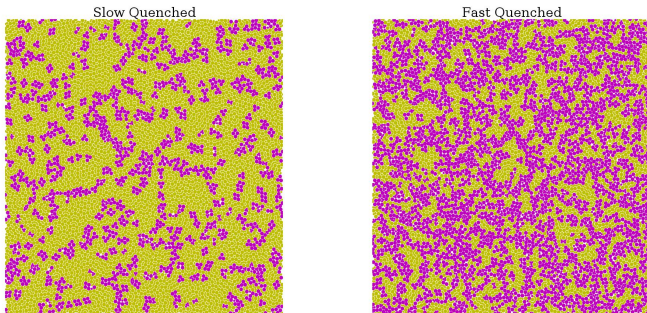
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Motifs are colored **yellow** and defects colored **magenta**.

- ▶ Such **slow quenched** glasses deform via shear bands!

## Deformation at zero temperature

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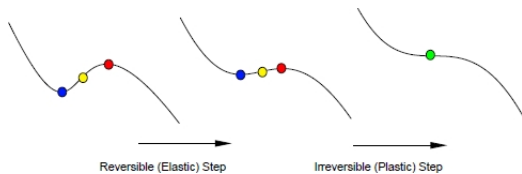
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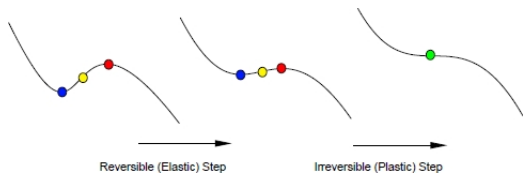
- ▶  $\mathbf{u}_i$  is necessary to restore equilibrium in amorphous materials.
- ▶ This also guarantees:  $\underbrace{\mathbf{v}}_{\text{non-affine velocity}} = - \underbrace{\mathbf{H}^{-1}}_{\text{Inverse Hessian}} \cdot \underbrace{\mathbf{\Xi}}_{\text{affine force}}$

# Elementary plastic instability

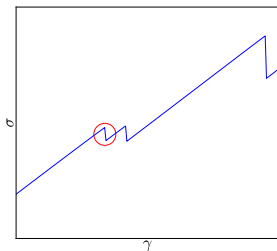


- ▶ At some  $\gamma = \gamma_p$ , a **saddle point** emerges.

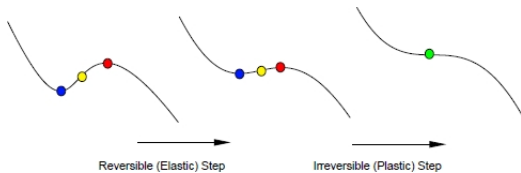
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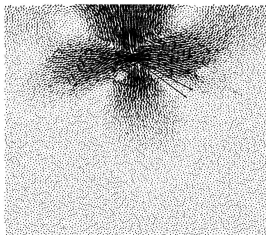
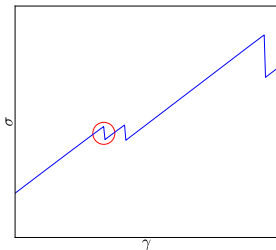
- ▶ At some  $\gamma = \gamma_p$ , a **saddle point** emerges.
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- ▶ Corresponding wave-function gets **localized**.



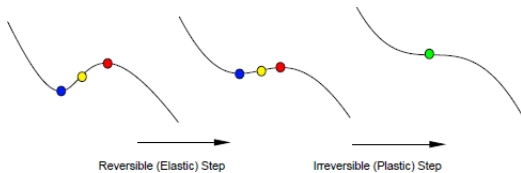
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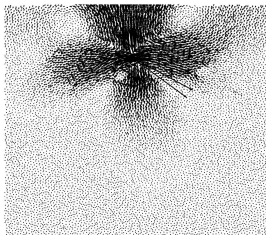
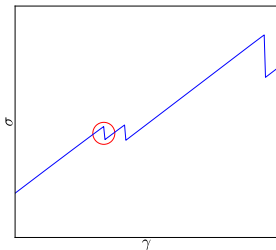
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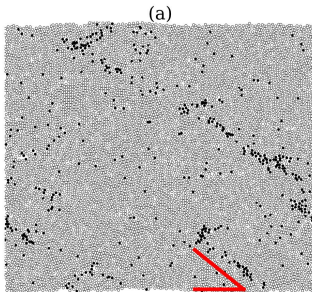
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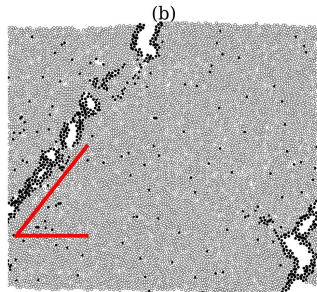
# Uniaxial deformation

## Instability

- ▶ Strain localizes into thin regions or **shear bands**.
- ▶ Angle  $\theta$  w.r.t principal axis is **higher** in extension.



(a) Compression:  $\theta = 46^\circ$

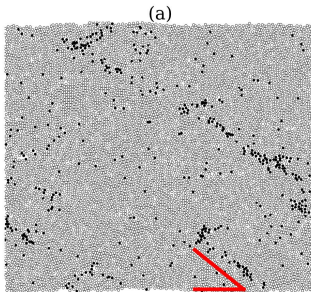


(b) Extension:  $\theta = 54^\circ$

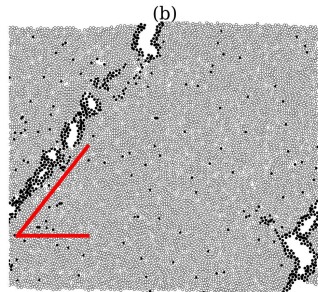
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Next we will construct a theory for both these asymmetries.

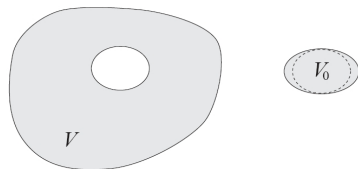


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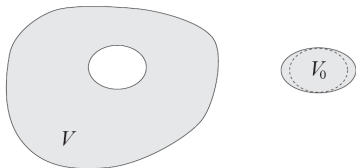
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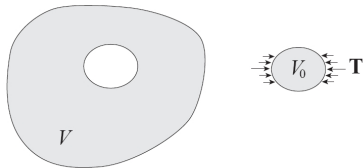
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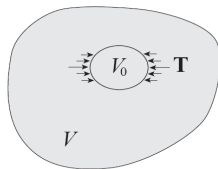
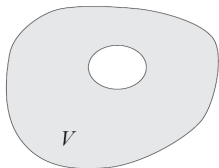
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(2) Apply surface traction to make the inclusion return to its original shape.

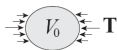
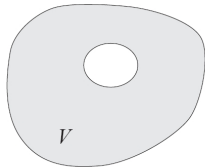
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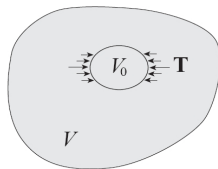
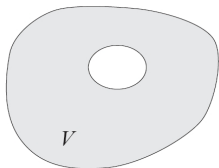
(3) Put the inclusion back into the matrix.



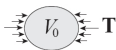
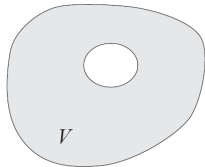
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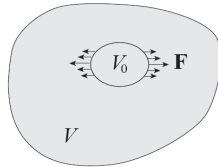


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# Characteristics of Eshelby inclusion

- ▶ Eigenstrain tensor

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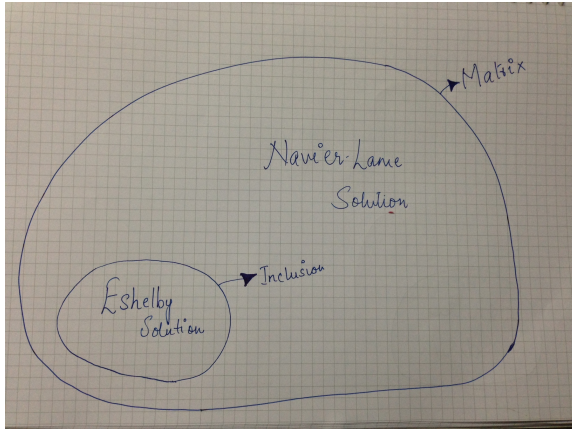
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- ▶  $\epsilon_{\eta\eta}^* \neq 0$  as volume is allowed to change.
- ▶ In general, the ratio  $\zeta_n/\zeta_k$  depends on loading protocols.
- ▶  $\zeta_n/\zeta_k$  uniquely determines the shear-band angle.



# Mathematical procedure



- ▶ Both solutions matched at the inclusion boundary:

$$\mathbf{u}^c(\mathbf{X}) \equiv \mathbf{u}^c(\zeta_n, \zeta_k, \lambda, \mu, a, \hat{\mathbf{n}}, \mathbf{X})$$

# Energy contributions

To calculate the total energy we must calculate

$$E_{mat} = \frac{1}{2} \sigma_{\alpha\beta}^{\infty} \epsilon_{\beta\alpha}^{\infty} V \quad \text{"Energy of the strained matrix"}$$

$$E_{\infty} = -\frac{1}{2} \sigma_{\alpha\beta}^{\infty} \sum_{i=1}^{\mathcal{N}} \epsilon_{\beta\alpha}^{*,i} V_0^i \quad \text{"Energy of inclusions"}$$

$$E_{esh} = \frac{1}{2} \sum_{i=1}^{\mathcal{N}} (\sigma_{\alpha\beta}^{*,i} - \sigma_{\alpha\beta}^{c,i}) \epsilon_{\beta\alpha}^{*,i} V_0^i \quad \text{"Self energy required to create the inclusions"}$$

$$E_{inc} = -\frac{1}{2} \sum_{i=1}^{\mathcal{N}} \epsilon_{\beta\alpha}^{*,i} V_0^i \sum_{j \neq i} \sigma_{\alpha\beta}^{c,j} (r^{ij}) \quad \text{"Interaction energy between inclusions"}$$

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The total energy of  $\mathcal{N}$  such inclusions is thus

$$E = E_{mat} + E_{\infty} + E_{esh} + E_{inc}$$

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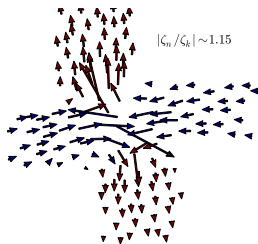
- ▶ Any other loading condition **will realize a different angle!**



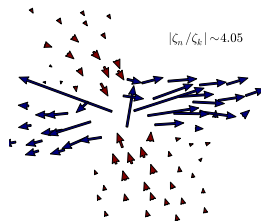
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To calculate  $\theta$ , we need the ratio  $\zeta_n/\zeta_k$

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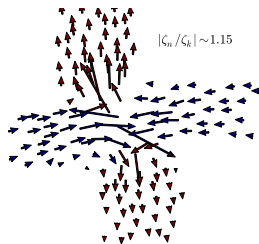
(b) Extension



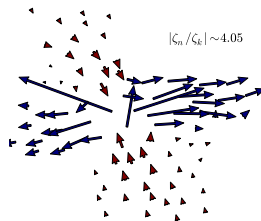
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Plugging the observed values of  $\zeta_n/\zeta_k$  in the angle formula:

$$\theta \approx 46^\circ \quad \text{for compression}$$

$$\theta \approx 54^\circ \quad \text{for extension}$$

# Limiting cases

## Agreement with experiments

- ▶ The two limiting cases result from our prediction

$$\theta = 30^0 \quad \text{for the case} \quad |\zeta_n/\zeta_k| \rightarrow 0$$

$$\theta = 60^0 \quad \text{for the case} \quad |\zeta_n/\zeta_k| \rightarrow \infty$$

- ▶ Available experimental data conform to this prediction

	Poisson's ratio	Fracture or shear-band angle (compression)	Fracture or shear-band angle (tension)
Pd <sub>40</sub> Ni <sub>40</sub> P <sub>20</sub>	0.403[12]	40.7–43.1[13], 42[14]	56[14]
Pd <sub>77.5</sub> Cu <sub>6</sub> Si <sub>16.5</sub>	0.411[12]	–	51[15]
Pd <sub>80</sub> Si <sub>20</sub>	0.33[16]	–	54.7[17], 48–50[18]
Zr <sub>40</sub> Ti <sub>14</sub> Ni <sub>10</sub> Cu <sub>12</sub> Be <sub>24</sub>	0.354[19]	42[19]	56[19]
Zr <sub>40</sub> Ti <sub>12</sub> Ni <sub>9.4</sub> Cu <sub>12.5</sub> Be <sub>26.4</sub>	0.35–0.37	39.5–43.7[20], 40[21]	53.3–60.7[20], 50–59[21]
Zr <sub>52.5</sub> Al <sub>10</sub> Ni <sub>10</sub> Cu <sub>13</sub> Be <sub>12.5</sub>	0.35–0.37	–	55[22]
Zr <sub>62</sub> Ti <sub>10</sub> Ni <sub>10</sub> Cu <sub>14.5</sub> Be <sub>3.5</sub>	0.35–0.37	39.5–43.7[23]	53.3–60.7[23]
Zr <sub>63.2</sub> Ti <sub>9.9</sub> Ni <sub>9.4</sub> Cu <sub>13.4</sub> Be <sub>4.1</sub>	0.35–0.37	39.4–41.4[21]	50–53[21]
Zr <sub>52.5</sub> Ni <sub>14.6</sub> Al <sub>10</sub> Cu <sub>17.9</sub> Ti <sub>5</sub>	0.35–0.37	40–45[24], 44–46[25], 42[26]	55–56[24], 53–58,[25] 56[26]
Zr <sub>54.5</sub> Ni <sub>8</sub> Al <sub>10</sub> Cu <sub>20</sub> Ti <sub>7.5</sub>	0.35–0.37	42[26]	–
Zr <sub>59</sub> Ni <sub>8</sub> Cu <sub>20</sub> Al <sub>10</sub> Ti <sub>3</sub>	0.35–0.37	42[27]	54[27], 54[26]
Zr <sub>55</sub> Ni <sub>3</sub> Cu <sub>30</sub> Al <sub>10</sub>	0.375[28]	40–43[26]	53–58[25]
Zr <sub>60</sub> Pd <sub>20</sub> Cu <sub>20</sub> Al <sub>10</sub>	–	–	50[29]
Zr <sub>65</sub> Ni <sub>10</sub> Al <sub>7.5</sub> Cu <sub>7.5</sub> Pd <sub>10</sub>	–	–	50[30]
Cu <sub>60</sub> Zr <sub>30</sub> Ti <sub>10</sub>	~0.36	–	54[31]
Ni <sub>78</sub> Si <sub>10</sub> B <sub>12</sub>	–	–	50–55[32]
Cu <sub>60</sub> Zr <sub>20</sub> Hf <sub>10</sub> Ti <sub>10</sub>	0.368[2]	40.5[33]	–
Fe <sub>70</sub> Ni <sub>10</sub> B <sub>20</sub>	~0.35	–	60[34]
Ni <sub>49</sub> Fe <sub>29</sub> P <sub>14</sub> B <sub>6</sub> Si <sub>2</sub>	0.37[35]	–	53[35]
Co <sub>70</sub> Si <sub>15</sub> B <sub>10</sub> Fe <sub>5</sub>	–	–	60[36]
Co <sub>43</sub> Fe <sub>20</sub> Ta <sub>8.5</sub> B <sub>31.5</sub>	–	44[37]	–
Fe <sub>57.6</sub> Co <sub>14.4</sub> B <sub>19.2</sub> Si <sub>4.8</sub> Nb <sub>4</sub>	–	44[38]	–
Al <sub>79.8</sub> Y <sub>8.55</sub> Ni <sub>4.75</sub> Co <sub>1.9</sub> Sc <sub>5</sub>	–	–	50[39]

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- ▶ Our theory captures these asymmetries through the characteristics of Eshelby inclusions.
- ▶ Loading protocols which conserve volume lead to  $\theta = 45^\circ$ .
- ▶ Any other protocol will realize a different angle.
- ▶ In our theory  $\theta$  is limited to lie between  $30^\circ - 60^\circ$ .
- ▶ Available experimental data conform to this prediction.

# Future Work

- ▶ The present atomistic theory is valid in limits  $\dot{\gamma} \rightarrow 0, T \rightarrow 0$ .
- ▶ We would like to include:
  - ▶ finite temperature effects,  $T \neq 0$ .
  - ▶ finite strain rate effects,  $\dot{\gamma} \neq 0$ .



**Thank You.**